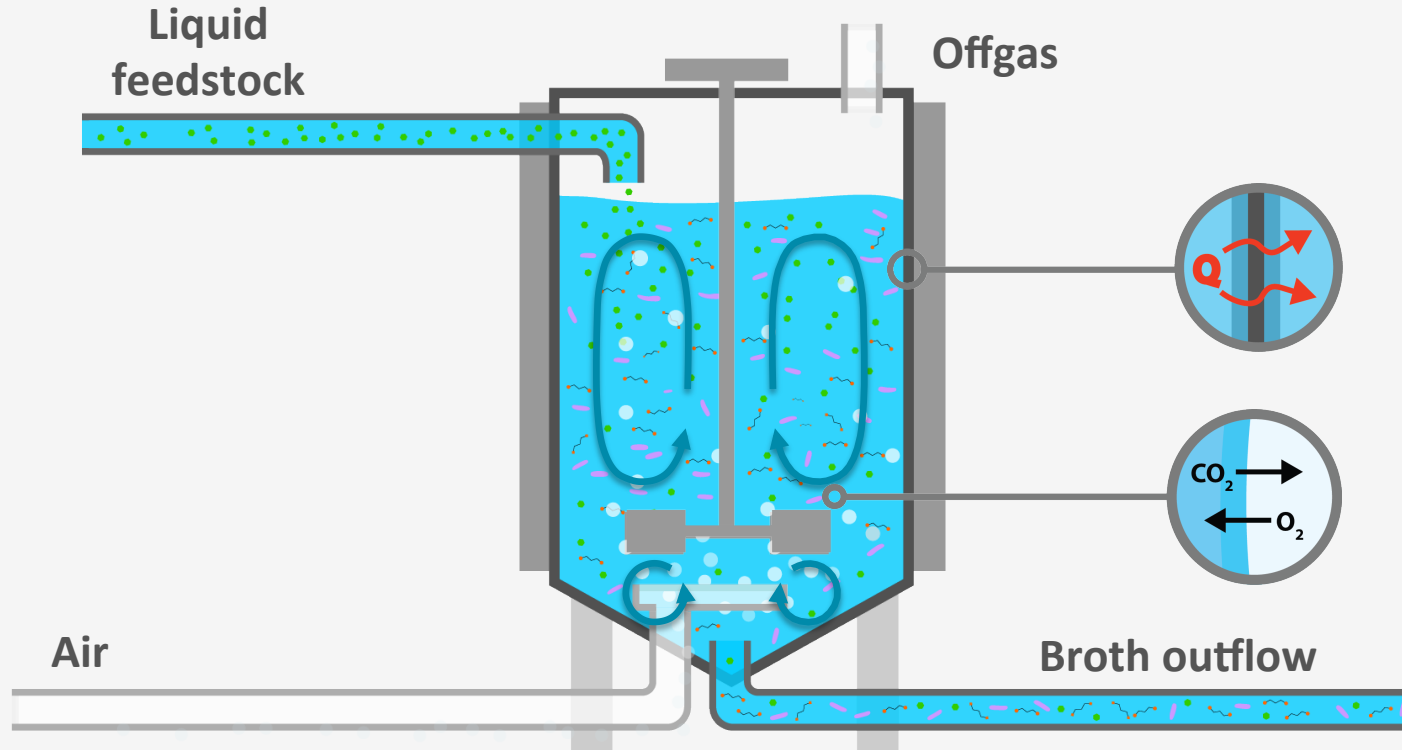


Mixing

Technology for biobased products

Henk Noorman, DSM / Department of Biotechnology, Faculty of Applied Sciences

One of four limiting transport steps: Mixing



Bubble column: liquid circulation patterns

Homogeneous \rightarrow heterogeneous
around superficial gas velocity of
0.04-0.08 m/s

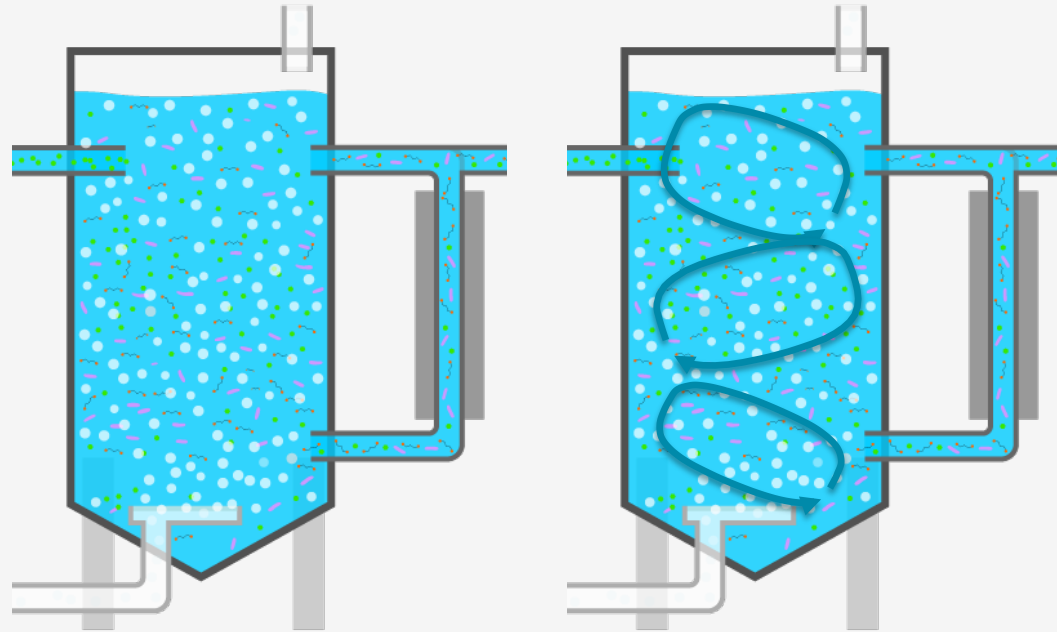
Remember the superficial gas
velocity? (m/s)

$$v_{gs} = \frac{F_g}{A_{\perp}}$$

Scale-up

At lab scale: often homogeneous

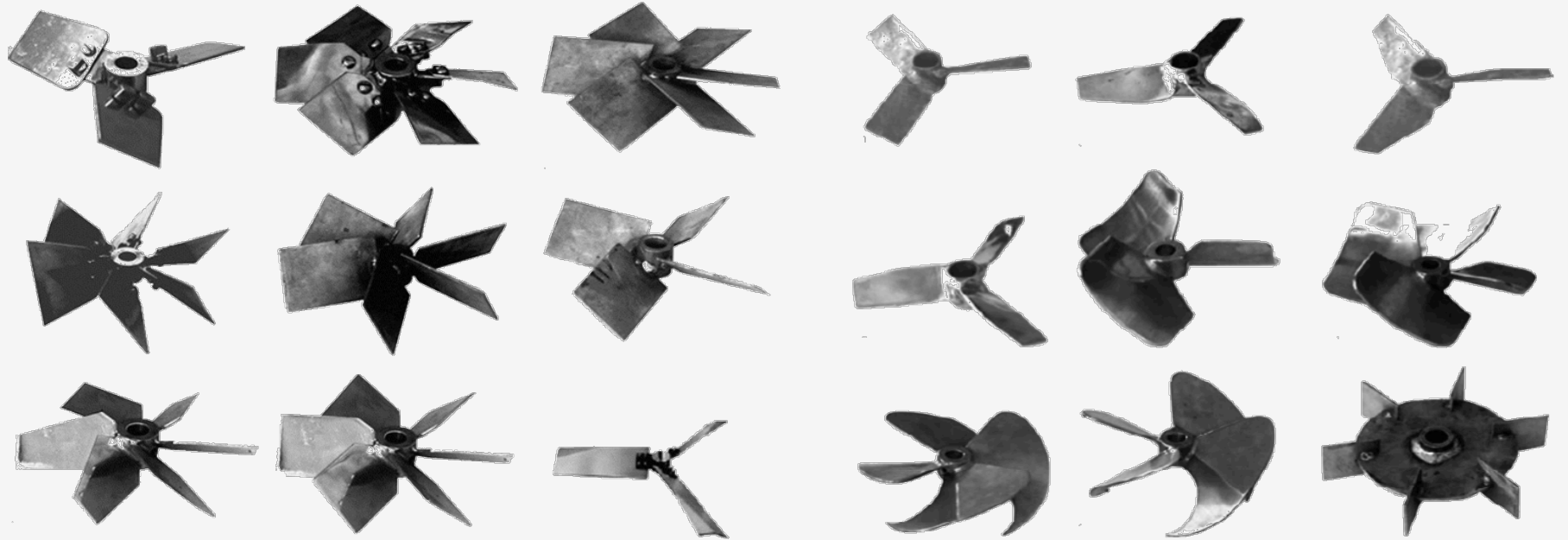
At full scale: heterogeneous



Homogeneous

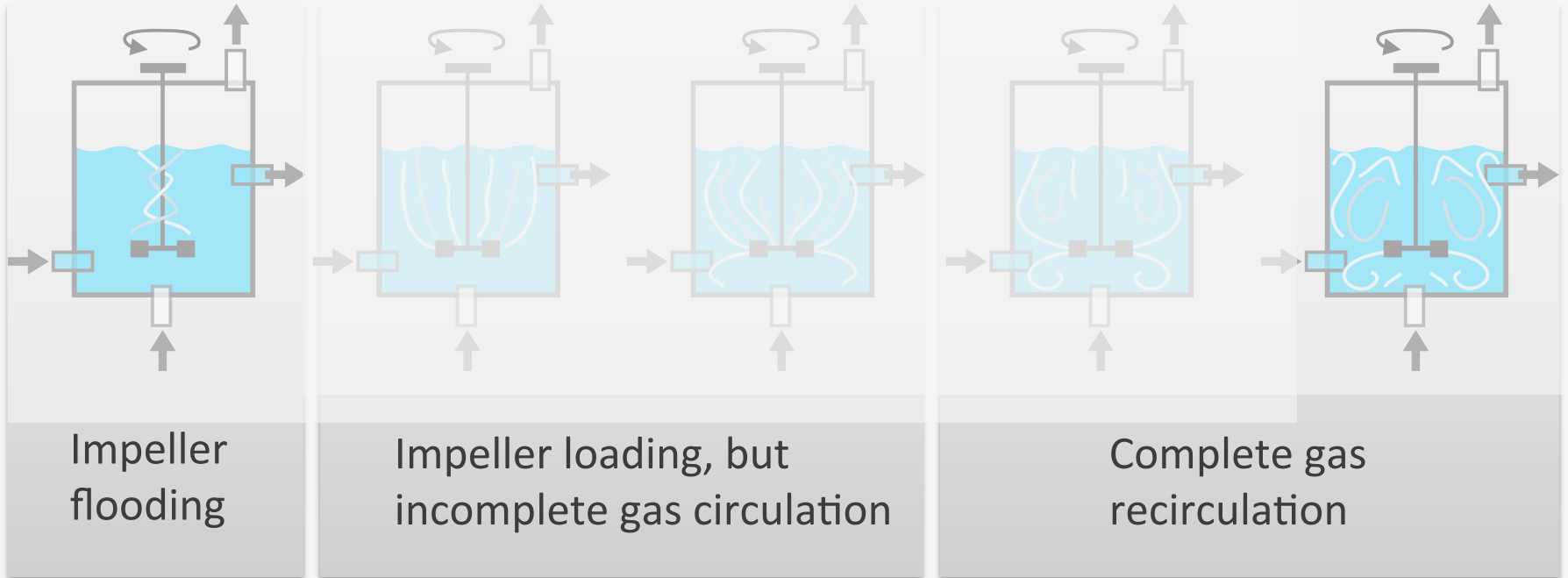
Heterogeneous

Stirred Tank Reactor (STR): Impeller designs

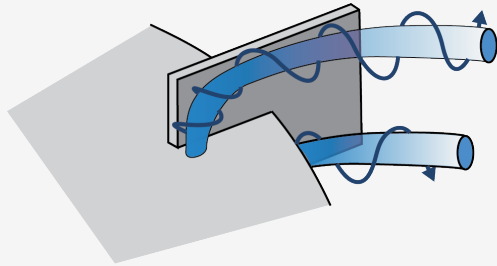


Gassed STR

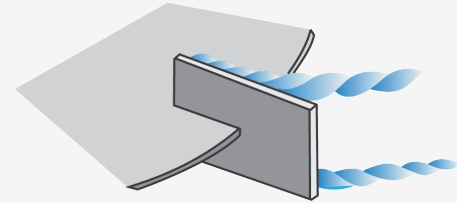
Impeller power input
(same gas flow rate)



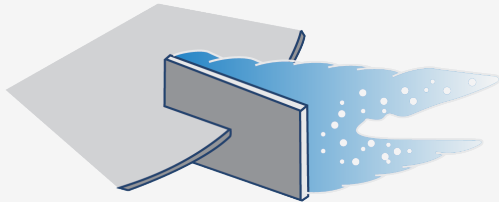
Gas dispersion



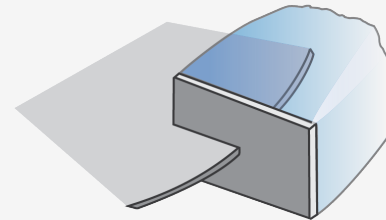
Unaerated



Vortex cavity

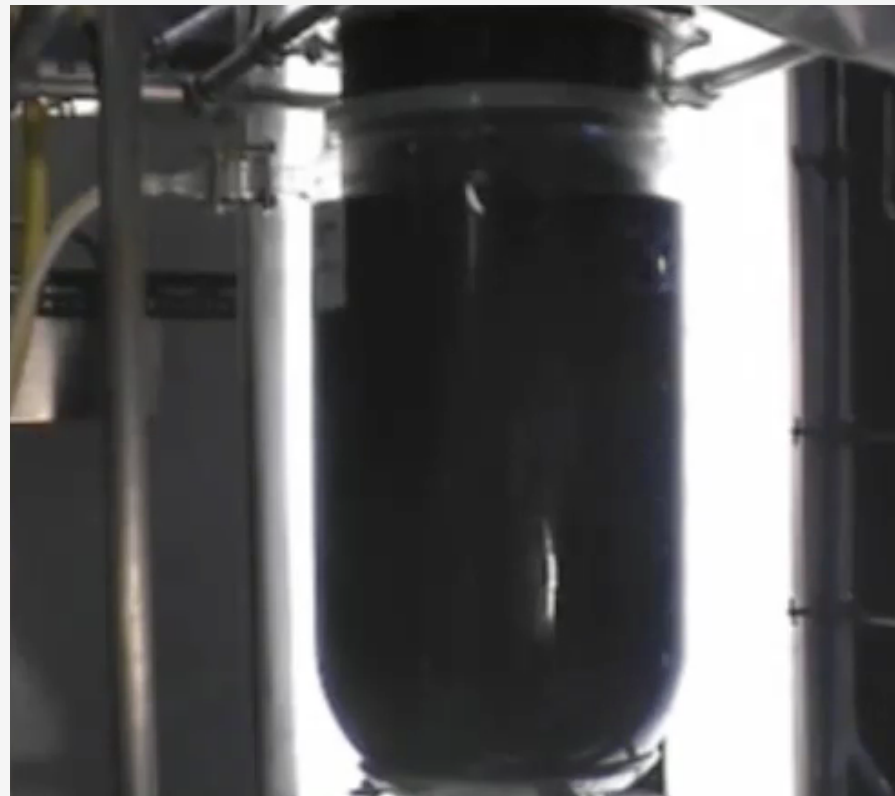


Clinging cavity

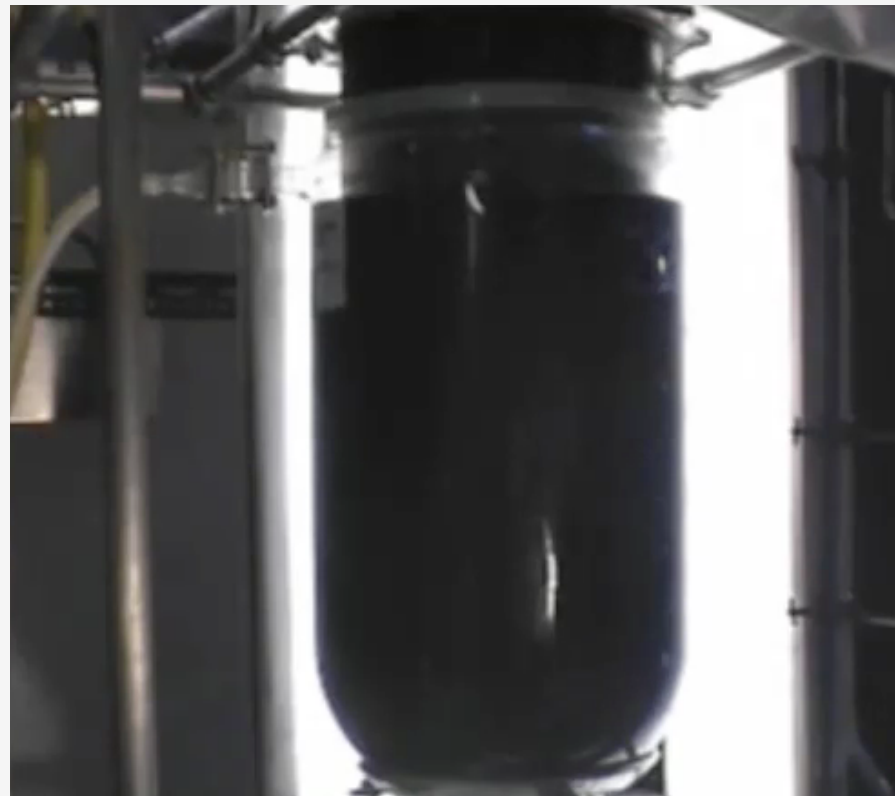


Large cavity

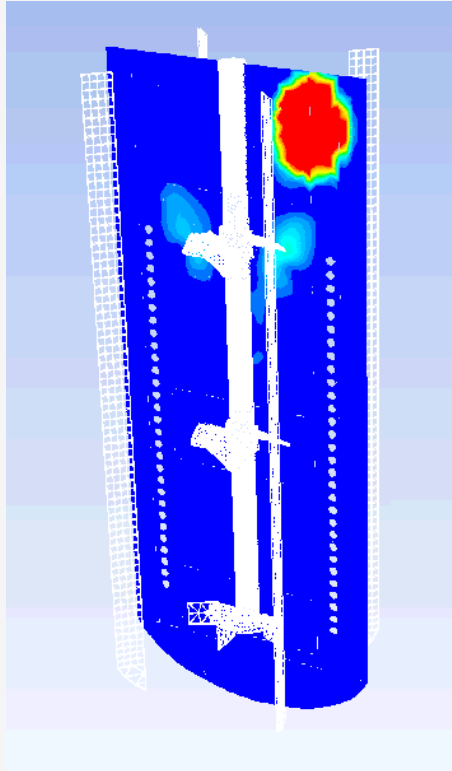
Mixing experiment



Mixing experiment



Computer simulation

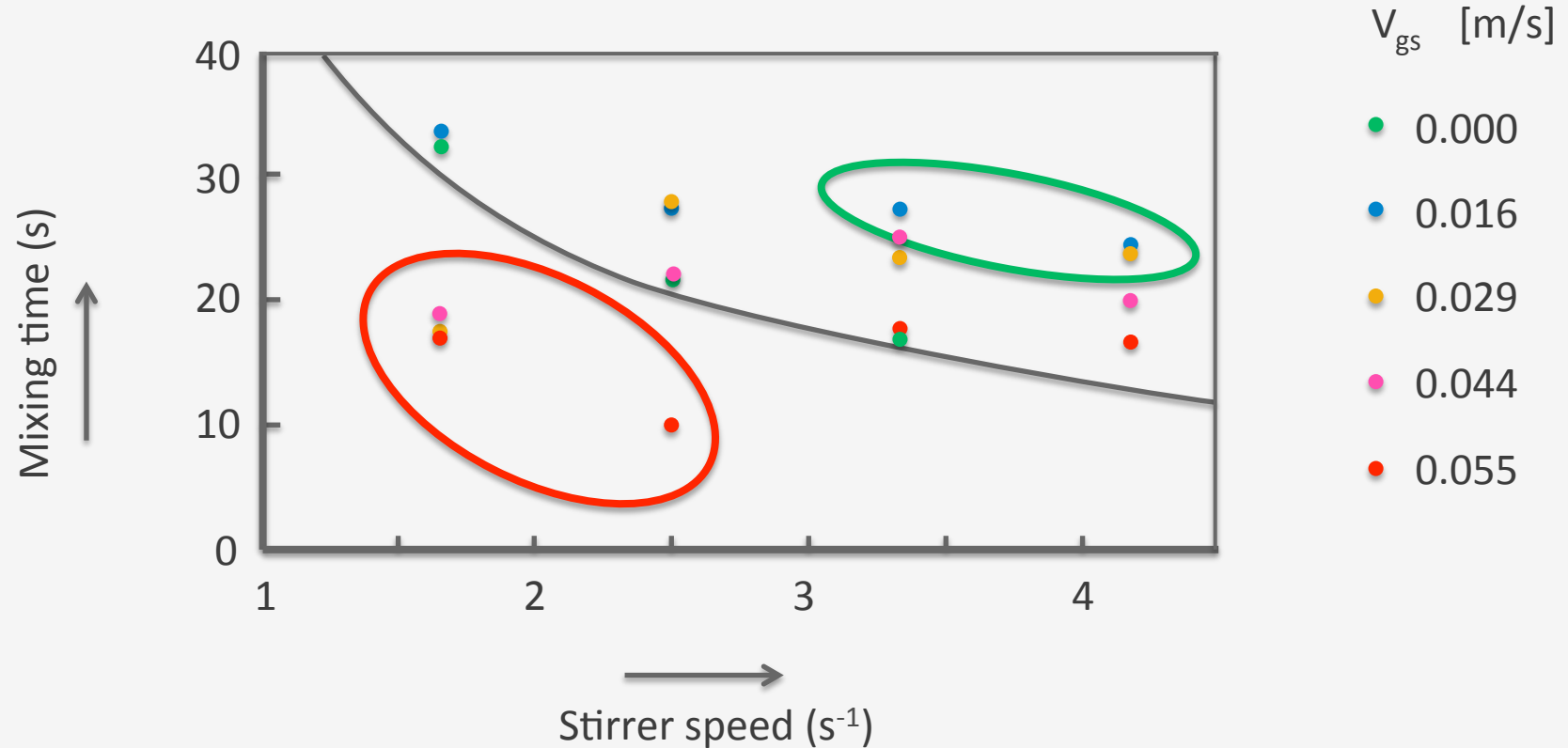


Mixing of tracer after injection

150 m³ bioreactor: 1 radial
and 2 axial impellers

95% mixing time 1 minute or more

The effect of aeration (30 m³ reactor)



Dimensionless mixing equation

Total power input (W/kg) ————┐
95% mixing time (s) ————┐
$$\text{Mixing number } N_{mix} = \frac{t_m e^{\frac{1}{3}}}{D^{\frac{2}{3}}} = \text{constant} \cdot \left(\frac{H}{D}\right)^2$$

Reactor diameter (m) ————┘

Constant for the same geometry and liquid flow regime

Aspect Ratio
Height/
diameter

! Constant for **specified geometries**
! Strongly dependent on **aspect ratio**

Van 't Riet, K, Van der Lans, RGJM, 2011. Mixing in bioreactor vessels. In: Comprehensive Biotechnology, Volume 2: 63-80 (2nd edition), Moo-Young (Ed.), Elsevier, Amsterdam

Comparison ALR, STR and BC

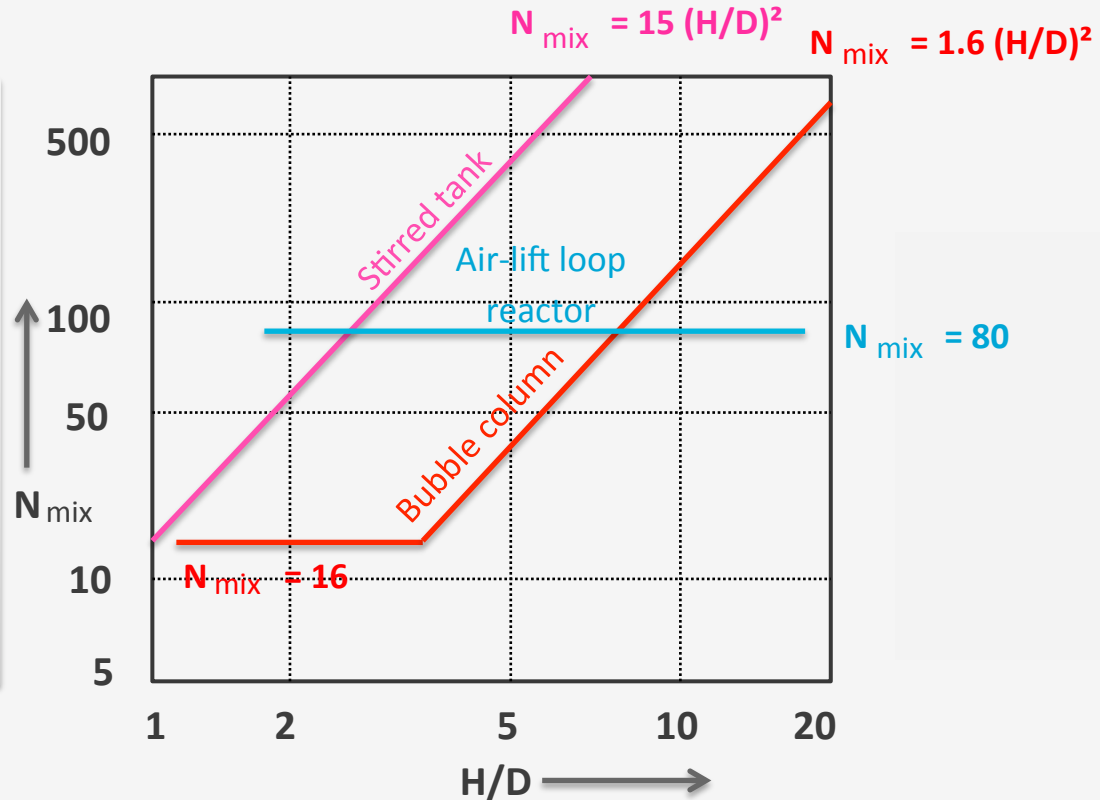
compared for 2 W/kg power input

Lower N_{mix} means better mixing!

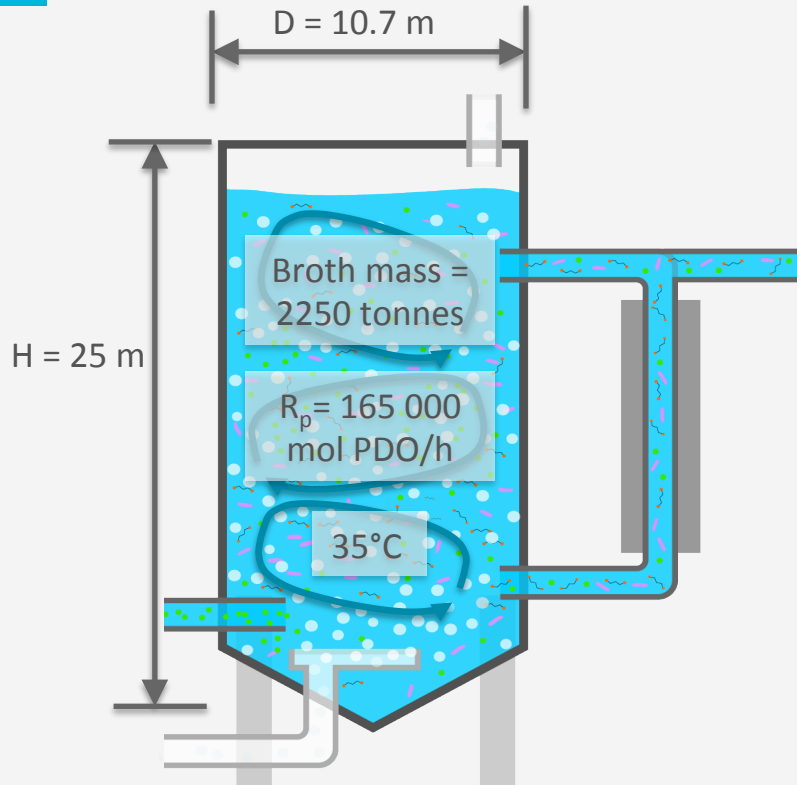
Low aspect ratio is favourable

At the same aspect ratio (H/D),
BC mixing is better than STR mixing

Mixing in an ALR is largely unaffected
by the aspect ratio



The PDO process scheme



Power input:

$$e = \frac{F_n RT \ln \left(\frac{p_{\text{bottom}}}{p_{\text{top}}} \right)}{\text{broth mass}}$$
$$= \frac{3561146 * 8.314 * 308 * \ln \left(\frac{3.5}{1} \right)}{2250000 / (3600 \text{ s/h})} = 1.41 \text{ W/kg}$$

Bubble column with $H/D = 2.34 \rightarrow N_{\text{mix}} = 16$

95% mixing time $t_{\text{mix}} = 16 \times 10.7^{2/3} / 1.41^{1/3} = 69 \text{ s}$

Mean broth circulation time $t_{\text{mix}}/4 = 17 \text{ s}$

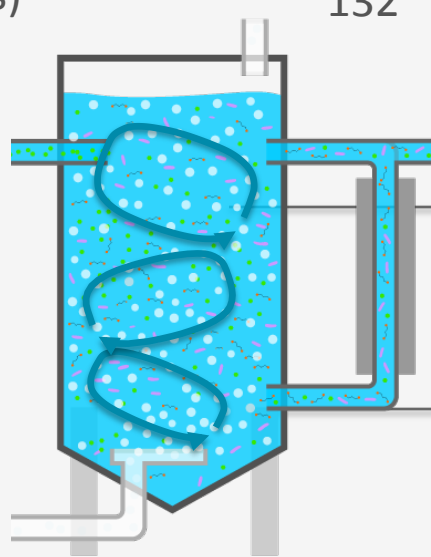
Mean broth circulation velocity $v_L = H / 17 = 1.5 \text{ m/s}$

Broth circulation rate $2250 / 17 = 132 \text{ m}^3/\text{s}$

Substrate concentration gradients

Concentration close to glucose feed inlet:

$$C_{s,\text{feed}} = \frac{F_{N,\text{glucose}} \text{ (mol/s)}}{F_{\text{circulation}} \text{ (m}^3\text{/s)}} = \frac{3 \times 71225 / 3600}{132} = 0.45 \text{ mol glucose / m}^3$$



Concentration in the outlet:

$$C_{s,\text{out}} = 0.085 \text{ mol glucose / m}^3$$

Mixing design

- BC: heterogeneous flow at full scale
- STR: several different flow regimes
- Low aspect ratios favourable for mixing
- Fewer (radial) stirrers better for mixing
- Aeration has minor influence at usual regime
- BC often better than STR
- ALR independent of aspect ratio

See you in the next unit!